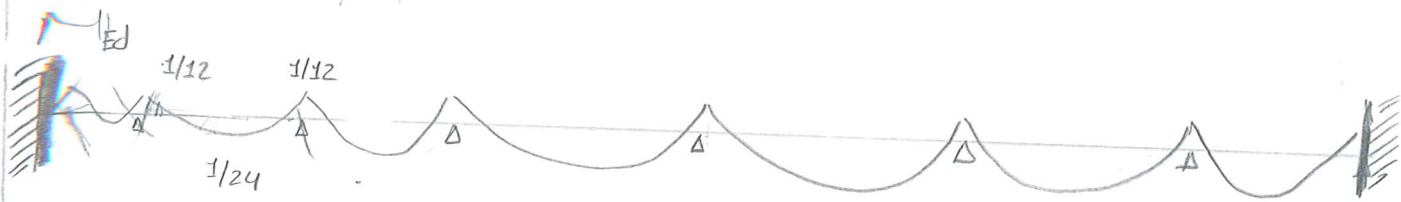
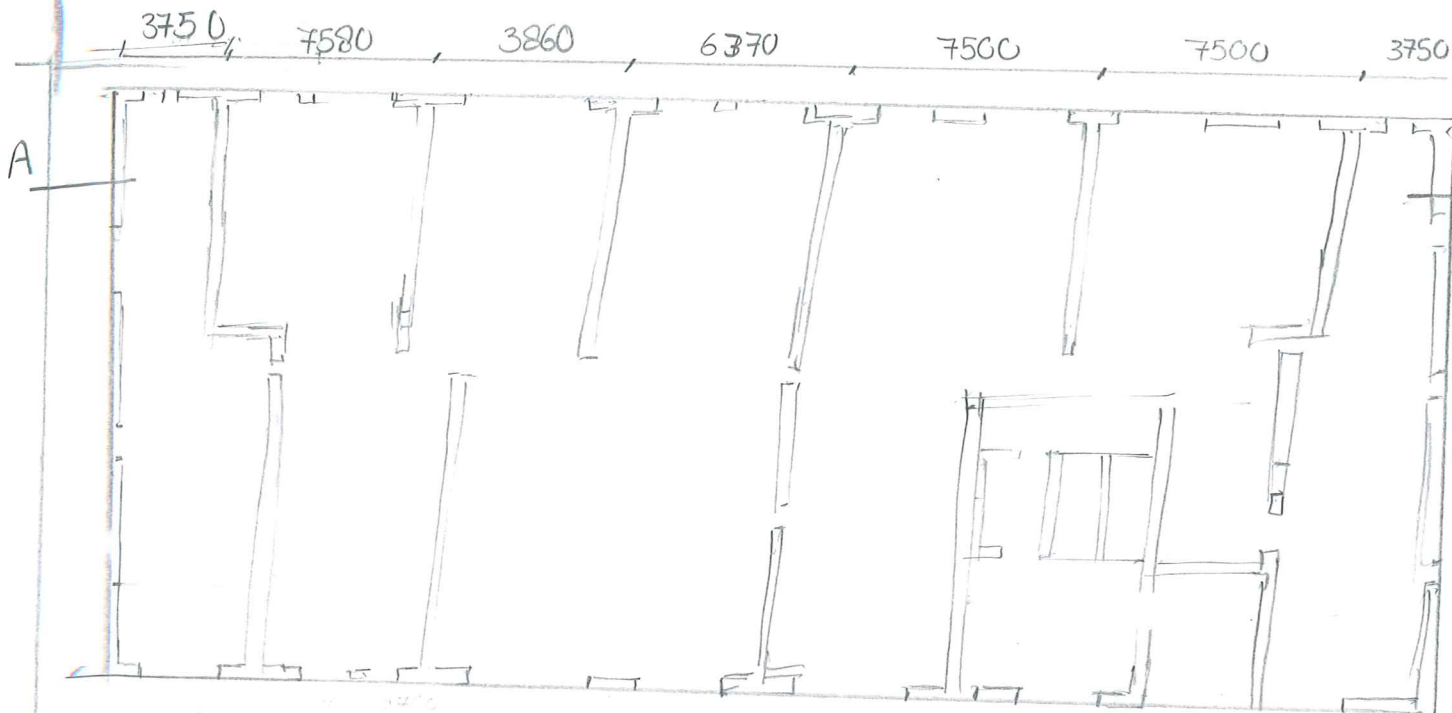


Design of Reinforced Concrete Slab: One-way



* Maximum Span 7500 mm

$$* M_{ED1} (\text{Top Reinforcement}) = \frac{1}{12} (F)(L)^2 = \frac{1}{12} (13,65)(7,5)^2 = 63,98 \text{ KN.m}$$

$$* M_{ED2} (\text{Bot Reinforcement}) = \frac{1}{24} (F)(L)^2 = \frac{1}{24} (13,65)(7,5)^2 = 32 \text{ KN.m}$$

$$* \Delta = \frac{1}{384} \frac{(F)(L)^4}{EI} = \frac{1}{384} * \frac{(9,81)(7500)^4}{30000 * (1,01 * 10^9)} = 2,67 \text{ mm}$$

$$* I = \frac{1}{12} (b)(h)^3 = \frac{1}{12} (1000)(230)^3 = 1,01 * 10^9 \text{ mm}^4$$

* Coefficient of Creep & Shrinkage $\gamma = 4$ (28-34)

$$* \text{Long Term Deflection} = \gamma * (\Delta) = 4 * 2,67 = 10,8 \text{ mm} < \frac{L}{250} = \frac{7500}{250} = 30 \text{ mm}$$

$$h = \frac{1}{3} * 7500 = 2500 \Rightarrow 230 \text{ mm}$$

∴ OK

Load Table : General Floor :

Name	Calculation	Ch. Load	ϕ_F	Design load
Dead Load				
Self Weight	$0,23 \times 25$	5,75	1,35	7,8
FLOORING		1,36	1,35	1,8
Sum(E)		7,11	1,35	9,6
Impose load				
Live load		1,5	1,5	2,25
Partition		1,2	1,5	1,8
Sum(E)		2,7	1,5	4,05
Sum(E)		9,81		13,65

$$\mu = \frac{M_{Ed1}}{b \cdot d^2 \cdot \eta \cdot F_{cd}} = \frac{(63,98 \cdot 10^6)}{1000 \cdot 199^2 \cdot 1 \cdot 20} = \underline{0,081}$$

$$d = 230 - 25 = \frac{b}{7} = \underline{199 \text{ mm}}$$

C30/37 \rightarrow $F_{ck} = 30 \text{ Mpa}$ \Rightarrow $F_{cd} = \frac{F_{ck}}{\gamma_c} = \frac{30}{1,5} = \underline{20 \text{ Mpa}}$

$$\xi = \underline{0,958}$$

$$A_{sreq} = \frac{M_{Ed1}}{\xi \cdot d \cdot F_{yd}} = \frac{(63,98 \cdot 10^6)}{0,958 \cdot 199 \cdot 435} = \underline{771,5 \text{ mm}^2}$$

Design of Reinforcement $\phi 10/100$; $A_{sprov} = 785 \text{ mm}^2 > A_{sreq} = 771,5 \text{ mm}^2$

\therefore OK

$$\mu = \frac{M_{Ed2}}{b \cdot d^2 \cdot \eta \cdot F_{cd}} = \frac{(32 \cdot 10^6)}{1000 \cdot 199^2 \cdot 1 \cdot 20} = \underline{0,040}$$

$$\xi = \underline{0,980}$$

$$A_{sreq} = \frac{M_{Ed2}}{\xi \cdot d \cdot F_{yd}} = \frac{(32 \cdot 10^6)}{0,980 \cdot 199 \cdot 435} = \underline{377 \text{ mm}^2}$$

Design of the Reinforcement $\phi 10/200$; $A_{sprov} = 393 \text{ mm}^2 > A_{sreq} = 377 \text{ mm}^2$

Design of Underground Level - Column :

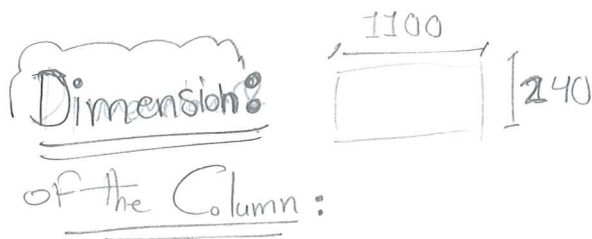


Load Area = $7,5 * 4,875 = 36,5 \text{ m}^2$

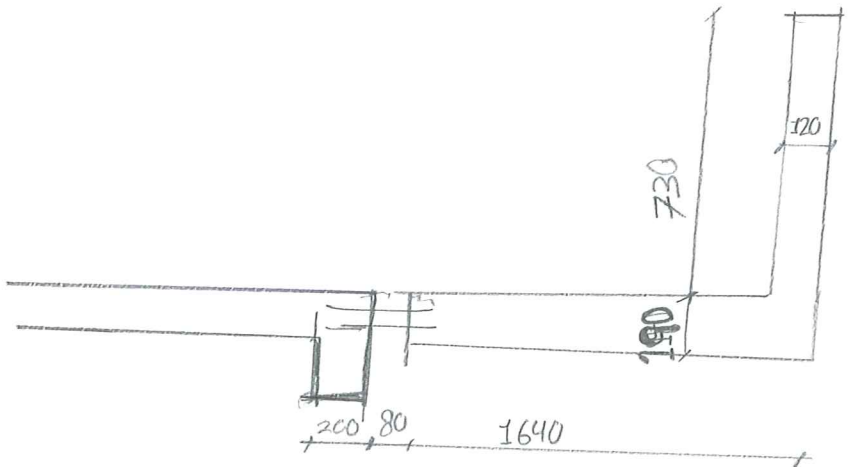
$$N_{Ed} = \underbrace{(13,65 * 6 * 36,5)}_{\text{Floors}} + \underbrace{(0,24 * 1,1 * 3 * 25)}_{\text{self weight of column}} + \underbrace{(0,22 * 4 * 15 * 25)}_{\text{Reinforced Concrete wall}} = 3339,2 \text{ kN}$$

$$N_{Rd} = A_c * F_{cd} + 0,02(A_c) * F_{yk} * 0,8 = (240 * 1100 * 20) + 0,02 * 240 * 1100 * 400 * 0,8$$

$$N_{Rd} = 6969,6 \text{ kN} > N_{Ed} = 3339,2 \text{ kN} \therefore \text{OK}$$



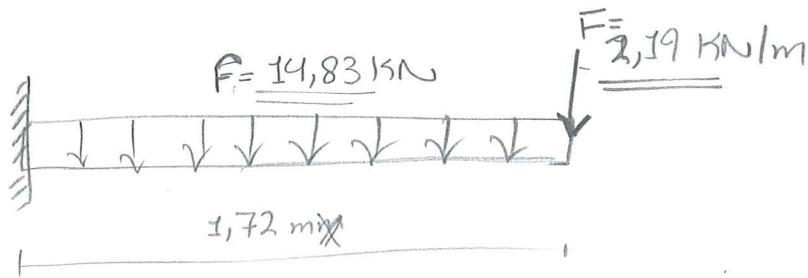
Design of Balcony RC Slab:



Name	Calculation	ch-Load	γ_F	Design Load
Dead Load				
Self Weight	$0,19 * 25$	4,75	1,35	6,41
FLOORING		1,79	1,35	2,42
SUM(Σ)		6,54		8,83
Impose Load				
Live Load		3	1,5	4,5
Snow Load		1	1,5	1,5
Sum(Σ)		4		6,0
Sum(Σ)		10,54		14,83

Preped load : $0,12 * 0,73 * 25 = \underline{\underline{2,19 \text{ KN/m}}}$

Structure Scheme of Balcony:



$$M_{Ed} = \frac{1}{2} (F)(L)^2 + F \cdot L = \frac{1}{2} (14,83)(1,72)^2 + (2,19)(1,72) = \underline{25,7 \text{ kNm}}$$

$$V_{Ed} = 14,83 \cdot 1,73 + 2,19 = \underline{27,7 \text{ kN}}$$

Schöck Isokorb type **D**:

D20 M... VV6

$$M_{RD} = \underline{28,7 \text{ kNm}} \checkmark$$

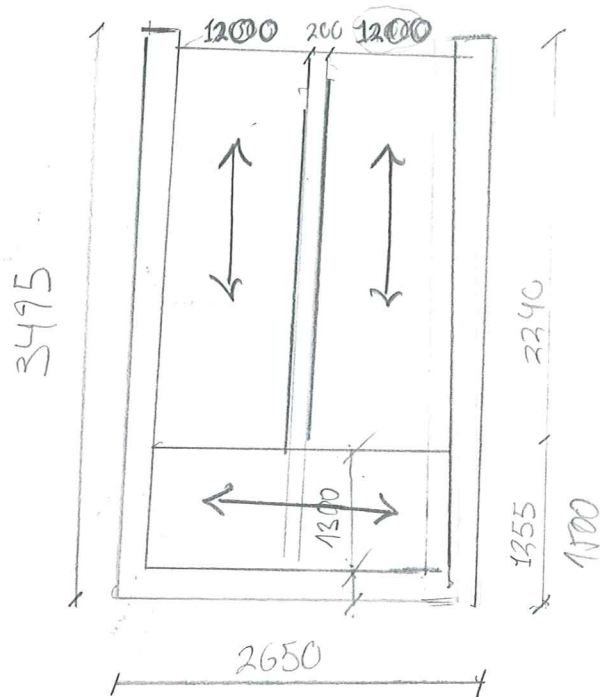
$$V_{RD} = \underline{52 \text{ kN}} \checkmark$$

Design Geometry of the Stair Case :

- Height of the Floor : $h_k = 3000 \text{ mm}$
- Depth of the Main Slab : $h_s = 230 \text{ mm}$
- Depth of the Floor Structure : $h_f = 130 \text{ mm}$
- Thickness of Cladding of the Stairs : $h_c = 15 \text{ mm}$

Dimension of the Stair Case :

- Ideal height of One Step is : 170 mm
- $3000/170 = 17,65 \Rightarrow 18 \text{ steps}$
- Height of Step $h = 3000/18 = 166,7 \text{ mm}$
- Width of One Step $b = 630 - 2h = 630 - 2(166,7) = 296,6 \text{ mm}$
- Design : Stair Case with $166,7/280 \text{ mm}$ Steps ... 2 flights, 9 steps in Each flight
- Width of the Flight : 1200 mm
- Width of the gap between flight : 200 mm
- Width of the Landing : 1255 mm
- Width of Stair Case : $1200 * 2 + 200 = 2600 \text{ mm}$
- Slope Of the Stair Case : $\alpha = \arctan(166,7/280) = 34,19^\circ$



Primary check of the depth of the Slab:

▣ The Stair Case is Considered in one-way Slab with span 2720 mm

The Slab will be Simply Supported \Rightarrow The depth should be atleast

$$2720/25 = 108,8 \text{ mm}$$

▣ The depth of Landing = 190 mm

▣ The depth of Flight = 140 mm

▣ 140 mm > 108,8 mm \Rightarrow OK

Perpendicular & head Clearance of the Stair Case:

□ Head Clearance of the Stair Case Should be More than $1500 + 750 / \cos \alpha$
 $= 1500 + 750 / \cos(34,19) = 2371 \text{ mm} \text{ \& more than } 2100 \text{ mm}$

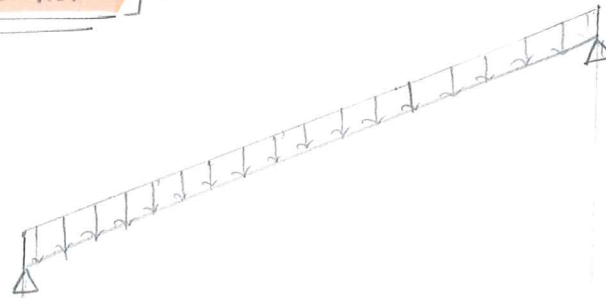
□ Head Clearance of Our Stair Case is $h_1 = h_k - h_s - h_p - h = 3000 - 230 - 130 - 166$

$h_1 = 2474 \text{ mm} \Rightarrow h = 2371 \text{ mm} \therefore \text{OK}$

□ Perpendicular Clearance of Stair Case Should be More than
 $750 + 1500 * \cos(\alpha) = 750 + 1500 * \cos(34,19) = 2038 \text{ mm} \text{ \& more than } 1900 \text{ mm}$

□ $h_2 = h_1 \cos \alpha = 2474 * \cos(34,19) = 2125 \text{ mm} \therefore \text{OK}$

Structure Scheme:



Dead load: $(0,165 * 25) + \left(\frac{0,167 * 25}{2}\right) + (0,015 * 2 * 20) = 6,8 \text{ kN/m}^2$

Live Load: 3 kN/m^2

$F_{DF} = (F_d * 1,35) + (F_L * 1,5) = (6,8 * 1,35) + (3 * 1,5) = 13,68 \text{ kN/m}^2$

$M_{ED} = \frac{1}{12} F_{DF} L^2 = \frac{1}{12} (13,68) (2240)^2 = 8,7 \text{ kN!m/m}$

$$d = \frac{140 - 25 \cdot 10}{2}$$

$$d = 110 \text{ mm}$$

$$M = \frac{M_{ED}}{b \cdot d^2 \cdot \eta \cdot F_{cd}} = \frac{(5,7 \cdot 10^6)}{1000 \cdot 110^2 \cdot 1 \cdot 20} = 0,024$$

$$\xi = 0,99$$

$$A_{s,req} = \frac{M_{ED}}{\xi \cdot d \cdot F_{yd}} = \frac{(5,7 \cdot 10^6)}{0,99 \cdot 110 \cdot 435} = 120 \text{ mm}^2$$

Design of the Reinforcement: $\phi 8/200$; $A_{s,prov} = 251 \text{ mm}^2 > A_{s,req} = 120 \text{ mm}^2$